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A Two-Machine Repair Model with Variable Repair Rate

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Abstract

A two-unit cold standby production-system with one repairman is considered. After inspection of a failed unit the repairman chooses either a slow or a fast repair rate to carry out the corresponding amount of work. At system-breakdown the repairman has an additional opportunity to switch to the fast rate. If there are no fixed costs associated with system breakdowns, then the policy which minimizes long-run average costs is shown to be a two-dimensional Control Limit Rule. If fixed costs are incurred every time the system breaks down, then the optimal policy is not necessarily of Control Limit type. This is illustrated by a counterexample. Furthermore we present several performance measures for this maintenance system controlled by a two-dimensional Control Limit Rule.

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1 Introduction

In the classical machine repair problem there is a pool of repairmen maintaining a finite number of machines. Since each repairman can serve only one machine at a time, an interference problem exists as soon as the number of machines requiring maintenance exceeds the number of repairmen available. The machine repair problem is also known as machine interference problem and as finite source queueing problem.

In this paper we focus on controlling a production system by adjusting the repair rate. Our system consists of two units and a single repairman. The system is considered to be 'up' if one unit is operating and the other one is either under repair or kept in spare position (cold

standby). At breakdown of the operational unit, this unit is sent into the repair facility to be repaired. The spare unit takes over the working position. The system goes 'down' if a unit is still under repair at breakdown of the other one. Then, at completion of the ongoing repair the repaired unit enters the operating position, a repair is started on the failed unit, and the overall system recovers to 'up' state.

After inspection of a failed unit the repairman knows how much work is to be performed. Then he has the option to choose either a slow or a fast repair rate to carry out this amount of work. When the system breaks down while the repairman is working at slow rate, he has an additional opportunity to switch to the fast rate.

In Section 2, we prove that if there are no positive fixed costs associated with overall system break-downs, then the policy which minimizes the long-run average costs is a two-dimensional Control Limit Rule (also called threshold policy). If fixed costs are incurred every time the system breaks down, then the optimal policy is not necessarily of Control Limit type. This is illustrated by an example where a 4-region policy is shown to be the optimal one. In Section 3, assuming a two-dimensional Control Limit Rule to be imposed on our system, we present explicit expressions from which the long-run average costs, all moments of system up- and down-times, and an additional number of operational characteristics can be calculated.

An extensive survey of papers on various types of machine repair problems that appeared since the 1976 survey of Pierskalla & Voelker [1976] can be found in Cho & Parlar [1991]. In many papers structural results are derived on optimal policies such that the long-run average costs are minimized. Systems are controlled for instance by reduction of the number of repairmen (e.g. Winston [1978], Albright [1980]); by opening or closing the repair-shop (e.g. Hatoyama [1977]); by taking operating units out for preventive maintenance (e.g. Kawai [1981], Hatoyama [1977]); etc.

Relatively few papers consider direct control of the repair rate of the repairmen (Crabill [1974], Winston [1977], Albright [1980], Weber & Stidham [1987], Karmeshu & Jaiswal [1981]). They all assume the repair rate to depend on the number of units that have broken down and are waiting for repair. A general conclusion is that the optimal repair rate is a non-decreasing function of the number of failed units. In these papers, however, failure- and repair-times are exponentially distributed; fixed costs related with changing the repair rate or with a system breakdown are not considered; and the repair rate is chosen independently of the actual amount of work that is to be performed. In our situation failure- and repair times have general probability distribution functions. We also investigate the influence of fixed costs on the structure of the optimal policy. Furthermore in our model we allow the repair rate to depend on both the number of failed units and on the amount of work to be carried out on the unit that is under repair.

Throughout this paper we make the following assumptions.

Assumption 1 The amount of work that is required to restore a failed unit into 'as good as new' condition, is known before the repair is started.

This amount of work becomes known after inspection of the unit. This information is used to decide whether to start a repair at fast or at slow rate. At system breakdown, the residual amount of work is equal to the original amount of work minus the amount of work carried out during operation of the last working unit.

Assumption 2 It is not possible to switch back to slow rate during a fast repair.

Assumption 3 The repairman returns to slow rate at completion of every repair.

Assumption 2 and 3 are explained by assuming that a regular maintenance crew is present permanently, working at a certain (slow) rate. If necessary, an additional crew is hired to increase the repair rate. The additional crew is hired on a contractual base for one repair-task only. So, even if two consecutive repairs have to be carried out at fast rate, a fixed cost is charged for each of them.

We use the following notation:

- σ_1 := slow repair rate,
- σ_2 := fast repair rate ($\sigma_2 > \sigma_1$),
- c_1 := variable cost rate for repairing at rate σ_1 ,
- c_2 := variable cost rate for repairing at rate σ_2 ,
- K_2 := fixed costs to start a repair at (or switch to) fast rate σ_2 ,
- c_d := variable cost rate during down time (e.g. loss of production),
- K_d := fixed costs at start of system down-period,
- L := lifetime of a unit (i.i.d. with general distribution function $F(l)$; $l \geq 0$; $F(0) = 0$),
- $\bar{F}(l) := 1 - F(l)$; $l \geq 0$,
- $\mu_L := \int_0^\infty l dF(l) < \infty$,
- W := amount of work for a repair (i.i.d. with general distribution function $G(w)$; $w \geq 0$),
- $\bar{G}(w) := 1 - G(w)$; $w \geq 0$,
- $\mu_W := \int_0^\infty w dG(w) < \infty$.

Now we make an additional assumption on the variable down costs c_d .

Assumption 4 There exists a policy with average costs (AC) less than c_d , i.e. $c_d > AC$.

If Assumption 4 is not fulfilled, then either the production system should be closed or the design should be adjusted to make the system profitable.

This paper is organized as follows. Section 2 considers the optimal control of the repair unit. First, in Section 2.1, we describe our system by a Semi Markov Decision Process. In Section 2.2,

we give a definition of a Control Limit Rule. Then, in Theorem 2.1, we show that at system-breakdown, the repair rate is switched to the fast rate σ_2 according to a Control Limit Rule. In the next two theorems we assume $K_d = 0$ (no fixed costs at system-breakdown). In Theorem 2.2, we prove that the repair rate to start a repair is chosen according to a Control Limit Rule. For the special case that no additional opportunity exists to switch to σ_2 at system-breakdown, in Theorem 2.3, we prove the repair rate to be chosen according to a Control Limit Rule as well. If $K_d > 0$, then the optimal rate to start a repair is not necessarily chosen according to a Control Limit Rule. This is illustrated by a counterexample in Section 2.3. Assuming a two-dimensional Control Limit Rule to be applied, in Section 3 we present performance measures such as long-run average costs, all moments of system up- and down-times, system availability, etc.

2 Optimal control

The repair rates are chosen such that the long-run average costs are minimized. While repairing at slow rate σ_1 (fast rate σ_2), a cost c_1 (c_2) per unit of time is incurred. Fixed costs K_2 are charged every time when either a fast rate σ_2 is chosen at the beginning of a repair, or when the repair rate is switched from σ_1 to σ_2 at the beginning of a down-period. Due to loss of production an additional variable cost rate c_d is incurred during down time. There are fixed costs K_d every time the system breaks down. Lifetimes (L) of the units are i.i.d. according to a general distribution function $F(l)$; $l \geq 0$ with finite mean μ_L . The amounts of work that have to be performed on failed units form a sequence of i.i.d. random variables with general distribution function $G(w)$; $w \geq 0$ with finite mean μ_W . Repaired units are ‘as good as new’.

2.1 Semi Markov Decision Process

The system is inspected at two types of decision epochs. Either when a new unit enters operation and a repair is started on the other one, or when the operating unit just failed and repair on the other unit has not been finished yet (system breakdown). Inspection reveals the system to be in a state $x \in \mathcal{X}$. The infinite *state-space* \mathcal{X} is defined by:

$$\mathcal{X} := \{(U, w), (D, \sigma_1, w), (D, \sigma_2, w); w \geq 0\},$$

where

- $U(D)$ denotes that a new repair is to be started (an ongoing repair has to be continued at system breakdown),
- σ_1, σ_2 denotes the current repair rate,
- w denotes the amount of work (still) to be carried out on the unit currently under repair.

If a new repair is started, then after inspection the repairman finds the system in a state (U, w) and has to choose either a slow or a fast rate to perform this repair. If the repairman is working at slow rate, then at system breakdown, he has to decide to continue working at slow rate or to switch to fast rate. Formally if at an inspection epoch the system is in state $x \in \mathcal{X}$, then the repairman has to choose an action $\sigma \in A(x)$. The finite *action-space* $A(x)$ is given by:

$$A(x) = \begin{cases} \{\sigma_1, \sigma_2\} & \text{if } x \in \{(U, w), (D, \sigma_1, w); w \geq 0\} \\ \sigma_2 & \text{if } x \in \{(D, \sigma_2, w); w \geq 0\}, \end{cases} \quad (2.1)$$

where

σ_1, σ_2 denotes the rate at which the current (residual) repair will be continued.

A *stationary* policy π is employed, i.e. the repair rate chosen depends on the present state of the system only:

$$\pi(x) \in A(x); x \in \mathcal{X}. \quad (2.2)$$

This controlled dynamic system is a Semi Markov Decision Process because the following properties are satisfied (cf. Tijms ([1986])). The time until, and the state at, the next decision epoch depend only on the present state $x \in \mathcal{X}$ and the chosen action $\sigma \in A(x)$, and are thus independent of the past history of the system. Also the costs incurred until the next decision epoch depend only on the present state and the action chosen in that state.

Let

- $\tau(x; \sigma) :=$ expected time until the next decision epoch, given that the current state of the system is $x \in \mathcal{X}$ and an action $\sigma \in A(x)$ is chosen.
- $c(x; \sigma) :=$ expected cost incurred during the time until the next decision epoch, given that the current state of the system is $x \in \mathcal{X}$ and an action $\sigma \in A(x)$ is chosen.
- $P(\cdot|x; \sigma) :=$ probability distribution of the state of the system at the next decision epoch, given that the current state of the system is $x \in \mathcal{X}$, and action $\sigma \in A(x)$ is chosen.

In Appendix A we show that, in case $G(\cdot)$ has finite support, there exists a bounded function $v(x)$, $x \in \mathcal{X}$ and a constant g , which satisfy the following set of *average cost optimality equations*.

$$v(x) = \min_{\sigma \in A(x)} \left\{ c(x; \sigma) - g\tau(x; \sigma) + \int_{y \in \mathcal{X}} v(y) dP(y|x; \sigma) \right\}; x \in \mathcal{X}. \quad (2.3)$$

According to Ross (Ross [1970]), for any policy which, when in state x , selects an action minimizing the right-hand side of (2.3), we have that the long-run average costs are minimized and are equal to g . So to find the optimal policy π^* we have to investigate which decision is to be made such that (2.3) is minimized.

In our model $\tau(x; \sigma)$ and $c(x; \sigma)$ are given by the following expressions:

$$\tau(D, \sigma_1, w; \sigma_1) = \frac{w}{\sigma_1},$$

$$\tau(D, \sigma_1, w; \sigma_2) = \frac{w}{\sigma_2},$$

$$\tau(D, \sigma_2, w; \sigma_2) = \frac{w}{\sigma_2},$$

$$\tau(U, w; \sigma_1) = \mu_L,$$

$$\tau(U, w; \sigma_2) = \mu_L,$$

$$c(D, \sigma_1, w; \sigma_1) = K_d + (c_1 + c_d) \frac{w}{\sigma_1},$$

$$c(D, \sigma_1, w; \sigma_2) = K_d + K_2 + (c_2 + c_d) \frac{w}{\sigma_2},$$

$$c(D, \sigma_2, w; \sigma_2) = K_d + (c_2 + c_d) \frac{w}{\sigma_2},$$

$$\begin{aligned} c(U, w; \sigma_1) &= c_1 \left[\int_0^{\frac{w}{\sigma_1}} l dF(l) + \frac{w}{\sigma_1} \bar{F}\left(\frac{w}{\sigma_1}\right) \right] \\ &= c_1 \left[\frac{w}{\sigma_1} - \int_0^{\frac{w}{\sigma_1}} F(t) dt \right], \end{aligned}$$

$$c(U, w; \sigma_2) = K_2 + c_2 \left[\frac{w}{\sigma_2} - \int_0^{\frac{w}{\sigma_2}} F(t) dt \right].$$

Substituting these expressions for $\tau(x; \sigma)$ and $c(x; \sigma)$ into (2.3), gives us the optimality equations for our Semi Markov Decision Process:

$$v(U, w) = \min \left\{ c_1 \left[\frac{w}{\sigma_1} - \int_0^{\frac{w}{\sigma_1}} F(t) dt \right] + \int_0^{\frac{w}{\sigma_1}} v(D, \sigma_1, w - \sigma_1 l) dF(l) + \bar{F}\left(\frac{w}{\sigma_1}\right) Z, \right. \quad (2.4)$$

$$\left. K_2 + c_2 \left[\frac{w}{\sigma_2} - \int_0^{\frac{w}{\sigma_2}} F(t) dt \right] + \int_0^{\frac{w}{\sigma_2}} v(D, \sigma_2, w - \sigma_2 l) dF(l) + \bar{F}\left(\frac{w}{\sigma_2}\right) Z \right\} - g \mu_L,$$

$$v(D, \sigma_1, w) = \min \left\{ (c_1 + c_d - g) \frac{w}{\sigma_1}, K_2 + (c_2 + c_d - g) \frac{w}{\sigma_2} \right\} + K_d + Z, \quad (2.5)$$

$$v(D, \sigma_2, w) = (c_2 + c_d - g) \frac{w}{\sigma_2} + K_d + Z, \quad (2.6)$$

where

$$Z := \int_0^\infty v(U, w) dG(w).$$

2.2 Control Limit Rule

From (2.1) we observe that there are two types of decision epochs in which an actual decision should be made: (U, w) and (D, σ_1, w) . (Due to Assumption 2 in (D, σ_2, w) the repair rate remains unchanged). For any stationary policy π , we define (cf. (2.2)):

$$\begin{aligned}\pi_U(w) &:= \pi(U, w), \\ \pi_D(w) &:= \pi(D, \sigma_1, w).\end{aligned}$$

Definition 2.1 For any stationary policy π , we call π_U a *Control Limit Rule* $\text{CLR}(m_U)$ if there exists some threshold value m_U such that:

$$\pi_U(w) = \sigma_2 \quad \text{iff } w > m_U.$$

□

For π_D a similar definition of $\text{CLR}(m_D)$ applies. If π_U is $\text{CLR}(m_U)$ and π_D is $\text{CLR}(m_D)$ then the overall system is controlled by a *two-dimensional Control Limit Rule* $\text{CLR}(m_U, m_D)$. The optimal policy is denoted by π^* with corresponding π_U^* and π_D^* .

In Theorem 2.1, we prove that in state (D, σ_1, w) the repair rate is switched from σ_1 to σ_2 according to a Control Limit Rule $\text{CLR}(m_D)$, no matter what (stationary) policy is followed in states (U, w) . For $K_d = 0$, and using the result of Theorem 2.1, we prove in Theorem 2.2 that in state (U, w) the fast rate σ_2 is chosen according to a Control Limit Rule $\text{CLR}(m_U)$ as well. In Theorem 2.3, we consider a restricted version of the model presented so far. In this adapted version we assume that it is not possible to change the repair rate during an ongoing repair. This means that in state (U, w) a repair rate is chosen which holds for the entire repair task. For such situations with $K_d = 0$, in Theorem 2.3 again we prove that the optimal rate is chosen according to a CLR. However, if $K_d > 0$ then the optimal policy in state (U, w) is not necessarily a CLR. A counterexample and an intuitive explanation are given in Section 2.3.

Theorem 2.1 π_D^* is a Control Limit Rule $\text{CLR}(m_D)$.

Proof: From (2.5) we conclude that σ_2 is chosen in state (D, σ_1, w) iff

$$\begin{aligned}K_2 + (c_2 + c_d - g) \frac{w}{\sigma_2} &< (c_1 + c_d - g) \frac{w}{\sigma_1} \quad \Leftrightarrow \\ w \left[\frac{c_1 + c_d - g}{\sigma_1} - \frac{c_2 + c_d - g}{\sigma_2} \right] &> K_2.\end{aligned}\tag{2.7}$$

If

$$\frac{c_1 + c_d - g}{\sigma_1} \leq \frac{c_2 + c_d - g}{\sigma_2}$$

then (2.7) will not hold for any $w \geq 0$. So, the repairman will never switch to σ_2 ($m_D := \infty$).

If

$$\frac{c_1 + c_d - g}{\sigma_1} > \frac{c_2 + c_d - g}{\sigma_2}$$

then σ_2 is chosen iff

$$w > m_D,$$

where

$$m_D := K_2 \left/ \left[\frac{c_1 + c_d - g}{\sigma_1} - \frac{c_2 + c_d - g}{\sigma_2} \right] \right. . \quad (2.8)$$

So, σ_2 is chosen according to a Control Limit Rule. \square

Remark 2.1 In Theorem 2.1 we have not used any information about the structure of the (stationary) policy employed in state (U, w) . Actually, assuming an arbitrary stationary policy to be employed in state (U, w) , one can construct an alternative Semi Markov Decision Process on the embedded states $\{(D, \sigma, w); w \geq 0, \sigma \in \{\sigma_1, \sigma_2\}\}$ only. From the corresponding optimality equations it is easy to see that the conditions for the repairman to choose σ_2 in state (D, σ_1, w) are similar to those found in the proof of Theorem 2.1. So, in state (D, σ_1, w) the repair rate is switched from σ_1 to σ_2 according to a Control Limit Rule $\text{CLR}(m_D)$, no matter what stationary policy is followed in state (U, w) . \square

In Theorem 2.1 we have shown that the best way of switching to σ_2 at the beginning of a down-period, is according to a CLR. Therefore, in Theorem 2.2 we assume π_D^* to be $\text{CLR}(m_D)$, where m_D is the optimal Control Limit in state (D, σ_1, w) , as defined by (2.8).

Theorem 2.2 *If $K_d = 0$ and either $\frac{c_1}{\sigma_1} \geq \frac{c_2}{\sigma_2}$ or $F(l)$ is IFR, then π_U^* is a Control Limit Rule $\text{CLR}(m_U)$.*

Proof: Consider the optimality equations (2.4) upto (2.6) with $K_d = 0$. First we substitute (2.6) into (2.4). By changing the order of integration, this simplifies the second minimization term of (2.4):

$$\begin{aligned} K_2 + c_2 \left[\frac{w}{\sigma_2} - \int_0^{\frac{w}{\sigma_2}} F(t) dt \right] + \int_0^{\frac{w}{\sigma_2}} v(D, \sigma_2, w - \sigma_2 l) dF(l) + \bar{F}\left(\frac{w}{\sigma_2}\right) Z = \\ K_2 + \frac{c_2}{\sigma_2} w + (c_d - g) \int_0^{\frac{w}{\sigma_2}} F(t) dt + Z. \end{aligned} \quad (2.9)$$

For the remainder of this proof we distinguish three cases.

$$\text{Case (i)} \quad \frac{c_1 + c_d - g}{\sigma_1} \leq \frac{c_2 + c_d - g}{\sigma_2}.$$

From the proof of Theorem 2.1 we know that in this case in state (D, σ_1, w) always σ_1 is chosen. In (U, w) there is even less reason to work at fast rate, as no variable down costs c_d are accounted (initially) and $K_d = 0$. So, one would expect σ_1 to be optimal in this case. This is just what happens. From (2.5) we see:

$$v(D, \sigma_1, w) = (c_1 + c_d - g) \frac{w}{\sigma_1} + Z. \quad (2.10)$$

Substitution of (2.10) into (2.4), and using (2.9) yields:

$$v(U, w) = \min_{\sigma_1, \sigma_2} \left\{ \frac{c_1}{\sigma_1} w + (c_d - g) \int_0^{\frac{w}{\sigma_1}} F(t) dt, K_2 + \frac{c_2}{\sigma_2} w + (c_d - g) \int_0^{\frac{w}{\sigma_2}} F(t) dt \right\} + Z - g\mu_L. \quad (2.11)$$

Now σ_2 is chosen iff

$$\begin{aligned} K_2 + \frac{c_2}{\sigma_2} w + (c_d - g) \int_0^{\frac{w}{\sigma_2}} F(t) dt < \frac{c_1}{\sigma_1} w + (c_d - g) \int_0^{\frac{w}{\sigma_1}} F(t) dt &\Leftrightarrow \\ (c_d - g) \int_0^{\frac{w}{\sigma_2}} F(t) dt + \left[\frac{c_1}{\sigma_1} - \frac{c_2}{\sigma_2} \right] w > K_2. \end{aligned} \quad (2.12)$$

However,

$$(c_d - g) \int_0^{\frac{w}{\sigma_2}} F(t) dt + \left[\frac{c_1}{\sigma_1} - \frac{c_2}{\sigma_2} \right] w \leq \left[\frac{c_1 + c_d - g}{\sigma_1} - \frac{c_2 + c_d - g}{\sigma_2} \right] w \leq 0. \quad (2.13)$$

By combining (2.12) and (2.13) we conclude that σ_1 is chosen for all $w \geq 0$ ($m_U = \infty$).

$$\text{Case (ii)} \quad \frac{c_1 + c_d - g}{\sigma_1} > \frac{c_2 + c_d - g}{\sigma_2} \text{ and } w \leq m_D.$$

As in the previous case (i), we note that if condition (ii) holds in a down state (D, σ_1, w) , then σ_1 is chosen (due to Theorem 2.1). Again we prove that σ_1 is optimal in (U, w) as well, which is intuitively clear. In (2.4) $v(D, \sigma_1, w - \sigma_1 l)$ only occurs for

$$0 \leq w - \sigma_1 l \leq w \leq m_D.$$

So, again (2.10) is to be substituted into (2.4). From (2.11) we see that σ_2 is chosen if (2.12) holds. However,

$$(c_d - g) \int_0^{\frac{w}{\sigma_2}} F(t) dt + \left[\frac{c_1}{\sigma_1} - \frac{c_2}{\sigma_2} \right] w \leq \left[\frac{c_1 + c_d - g}{\sigma_1} - \frac{c_2 + c_d - g}{\sigma_2} \right] m_D = K_2, \quad (2.14)$$

by Definition 2.8. Now again by combining (2.12) and (2.14) we conclude that σ_1 is chosen for all $w \geq 0$.

$$\text{Case (iii)} \quad \frac{c_1 + c_d - g}{\sigma_1} > \frac{c_2 + c_d - g}{\sigma_2} \text{ and } w > m_D.$$

In this situation a non-trivial Control Limit is to be expected. Furthermore in this case we will actually use the condition that either $\frac{c_1}{\sigma_1} \geq \frac{c_2}{\sigma_2}$ or $F(l)$ is IFR. From Theorem 2.1 we know that σ_2 is chosen in state $(D, \sigma_1, w - \sigma_1 l)$ iff

$$w - \sigma_1 l > m_D \quad \Leftrightarrow \quad 0 \leq l < (w - m_D)/\sigma_1,$$

and σ_1 is chosen otherwise. We use this result to simplify the first minimization term in (2.4):

$$\begin{aligned}
& \int_0^{\frac{w}{\sigma_1}} v(D, \sigma_1, w - \sigma_1 l) dF(l) + \bar{F}\left(\frac{w}{\sigma_1}\right) Z = \\
& \int_0^{\frac{w - m_D}{\sigma_1}} \left[K_2 + (c_2 + c_d - g) \frac{w - \sigma_1 l}{\sigma_2} + Z \right] dF(l) \\
& + \int_{\frac{w - m_D}{\sigma_1}}^{\frac{w}{\sigma_1}} \left[(c_1 + c_d - g) \frac{w - \sigma_1 l}{\sigma_1} + Z \right] dF(l) + \bar{F}\left(\frac{w}{\sigma_1}\right) Z = \\
& (c_2 + c_d - g) \frac{\sigma_1}{\sigma_2} \int_0^{\frac{w - m_D}{\sigma_1}} F(t) dt + (c_1 + c_d - g) \int_{\frac{w - m_D}{\sigma_1}}^{\frac{w}{\sigma_1}} F(t) dt + Z
\end{aligned} \tag{2.15}$$

After substitution of (2.9) and (2.15) into (2.4) we finally find that σ_2 is chosen iff

$$K(w) > CH(w), \tag{2.16}$$

where

$$\begin{aligned}
K(w) & := \int_0^{\frac{w - m_D}{\sigma_1}} [1 - F(t)] dt, \\
H(w) & := \int_{\frac{w}{\sigma_2}}^{\frac{w}{\sigma_1}} [1 - F(t)] dt, \\
C & := (c_d - g) / \left(\sigma_1 \left[\frac{c_1 + c_d - g}{\sigma_1} - \frac{c_2 + c_d - g}{\sigma_2} \right] \right).
\end{aligned} \tag{2.17}$$

Due to Assumption 4 $c_d > g$, and thus $C > 0$. From (2.16), it is easy to see that the optimal policy is CLR if $0 < C \leq 1$. We have not been able, however, to derive a similar *general* result for $C > 1$ without the additional assumptions of the Theorem. Furthermore, since C contains g , the condition $0 < C \leq 1$ cannot be checked beforehand, which makes it useless for practical purposes.

To obtain sufficient conditions, that guarantee the optimality of a CLR, we note that

$$\begin{aligned}
K(m_D) & = 0 \quad ; \quad \lim_{w \rightarrow \infty} K(w) = \mu_L > 0, \\
CH(m_D) & = C \int_{\frac{m_D}{\sigma_2}}^{\frac{m_D}{\sigma_1}} [1 - F(t)] dt \geq 0 \quad ; \quad \lim_{w \rightarrow \infty} CH(w) = 0.
\end{aligned}$$

So,

$$K(m_D) \leq CH(m_D) \quad ; \quad K(\infty) > CH(\infty). \tag{2.18}$$

This implies that $K(w)$ and $CH(w)$ intersect at least once; $K(w)$ lies below $CH(w)$ initially and exceeds $CH(w)$ finally. A first conclusion from (2.18) is that there exists some $0 \leq \bar{w} < \infty$, such that σ_2 is chosen for all $w > \bar{w}$.

From (2.16) and (2.18) we see that a *necessary* condition for a CLR to be optimal, is that $K(w)$ and $CH(w)$ intersect only once. A *sufficient* (not necessary) condition to guarantee this is:

$$K'(w) \geq CH'(w), \quad \text{for } w > S, \quad (2.19)$$

where $K'(w)$ and $H'(w)$ denote the derivatives of $K(w)$ and $H(w)$ respectively:

$$K'(w) := \frac{1}{\sigma_1} \left[1 - F\left(\frac{w-m_D}{\sigma_1}\right) \right] \geq 0, \quad (2.20)$$

$$H'(w) := \frac{1}{\sigma_1} \left[1 - F\left(\frac{w}{\sigma_1}\right) \right] - \frac{1}{\sigma_2} \left[1 - F\left(\frac{w}{\sigma_2}\right) \right] \in \mathbb{R}, \quad (2.21)$$

and

$$S := \text{first intersection point; } K(S) = CH(S); K'(S) > CH'(S).$$

A sufficient condition which guarantees (2.19) is:

$$\frac{c_1}{\sigma_1} \geq \frac{c_2}{\sigma_2}. \quad (2.22)$$

From (2.21) we see that in this case

$$\begin{aligned} CH'(w) &\leq C \left[\frac{1}{\sigma_1} - \frac{1}{\sigma_2} \right] \left[1 - F\left(\frac{w-m_D}{\sigma_1}\right) \right] \\ &= \left[\frac{c_1 + c_d - g}{\sigma_1} - \frac{c_2 + c_d - g}{\sigma_2} \right]^{-1} \left[\frac{c_d - g}{\sigma_1} - \frac{c_d - g}{\sigma_2} \right] \frac{1}{\sigma_1} \left[1 - F\left(\frac{w-m_D}{\sigma_1}\right) \right] \leq K'(w). \end{aligned}$$

So, if (2.22) holds then the optimal policy is CLR.

Another condition sufficient for (2.19) to hold, is that the lifetime distribution function with density function $f(l)$ is IFR, i.e. $F(l)$ has an Increasing Failure Rate:

$$\frac{f(x)}{1 - F(x)} \leq \frac{f(y)}{1 - F(y)} \quad \text{for } x < y, \quad (2.23)$$

which is explained as follows. From (2.17) and (2.21) we see:

$$H(0) = 0; \quad H'(0) > 0; \quad H(\infty) = 0.$$

In Lemma B.1 we prove that, if $F(l)$ is IFR then $H(w)$ is unimodal, i.e. $H(w)$ reaches its maximum in w_H^* (say) and

$$\begin{aligned} H'(w) &> 0 \quad \text{for } 0 \leq w < w_H^*, \\ H'(w) &< 0 \quad \text{for } w > w_H^*. \end{aligned}$$

If $S \geq w_H^*$ then (2.19) is certainly satisfied because $H'(w) < 0$ for $w > S$. If $S < w_H^*$ then consider

$$L(w) := \frac{K'(w)}{H'(w)} \quad \text{for } S < w < w_H^*.$$

Now (2.19) is satisfied if

$$L(w) > C \quad \text{for } S < w < w_H^*. \quad (2.24)$$

A sufficient condition to guarantee (2.24) is for $S < w < w_H^*$:

$$L'(w) \geq 0 \quad \Leftrightarrow$$

$$\frac{\frac{1}{\sigma_1} f\left(\frac{w-m_d}{\sigma_1}\right)}{1 - F\left(\frac{w-m_d}{\sigma_1}\right)} \leq \frac{\frac{1}{\sigma_1^2} f\left(\frac{w}{\sigma_1}\right) - \frac{1}{\sigma_2^2} f\left(\frac{w}{\sigma_2}\right)}{\frac{1}{\sigma_1} [1 - F\left(\frac{w}{\sigma_1}\right)] - \frac{1}{\sigma_2} [1 - F\left(\frac{w}{\sigma_2}\right)]},$$

which is satisfied if $F(l)$ is IFR. Thus (2.19) is satisfied, which is a sufficient condition for a CLR to be optimal. \square

In Theorem 2.2, the condition $\frac{c_1}{\sigma_1} \geq \frac{c_2}{\sigma_2}$ has an intuitively appealing interpretation. Repairing at rate σ_i costs c_i per unit of time, while σ_i units of work are performed per unit of time ($i = 1, 2$). Thus $\frac{c_i}{\sigma_i}$ denotes the cost of performing one unit of work at rate σ_i . If $\frac{c_1}{\sigma_1} \geq \frac{c_2}{\sigma_2}$ then working at fast rate σ_2 reduces both variable repair costs and the expected length of a down-period. Once w is so large that K_2 is sufficiently compensated by these reductions, there is no reason to believe σ_1 to become optimal again for larger values of w .

The case $\frac{c_1}{\sigma_1} < \frac{c_2}{\sigma_2}$ is less evident, because working at slow rate is cheapest. Both K_2 and the additional variable repair costs have to be fully compensated by a reduction of the expected down time. Once w and σ are given, the expected down time is determined by the lifetime distribution $F(l)$. Theorem 2.2 states that π_U^* is a Control Limit Rule if $F(l)$ is IFR, which is intuitively clear. We have not been able, however, to develop intuitive arguments to explain why a Control Limit Rule would not be optimal if both $\frac{c_1}{\sigma_1} < \frac{c_2}{\sigma_2}$ and $F(l)$ is non-IFR. Thus we conjecture that a CLR is optimal in (U, w) irrespective of the form of the lifetime distribution $F(l)$.

This conjecture is strengthened by Theorem 2.3, which considers a restricted model where the repair rate cannot be switched during an ongoing repair. This is equivalent with setting $m_D = \infty$ in the general model considered in Theorems 2.1 and 2.2. For this *restricted model* we prove in Theorem 2.3 that π_U^* is a CLR, without any limitations on either $F(l)$ or the variable cost rates.

Since the repair rate remains unchanged at system-breakdown, we have to consider embedded states (U, w) only. Thus we have to consider a modified Semi Markov Decision Process with corresponding state space \mathcal{X} and action space $A(x)$ given by:

$$\mathcal{X} := \{w; w \geq 0\},$$

$$A(x) := \{\sigma_1, \sigma_2\}, \quad x \in \mathcal{X}.$$

$\tau(x; \sigma)$ and $c(x; \sigma)$ are given by:

$$\begin{aligned} \tau(w; \sigma_1) &= \int_0^{\frac{w}{\sigma_1}} \frac{w}{\sigma_1} dF(l) + \int_{\frac{w}{\sigma_1}}^{\infty} l dF(l) \\ &= \frac{w}{\sigma_1} + \int_{\frac{w}{\sigma_1}}^{\infty} \bar{F}(t) dt, \end{aligned}$$

$$\begin{aligned}
\tau(w; \sigma_2) &= \frac{w}{\sigma_2} + \int_{\frac{w}{\sigma_2}}^{\infty} \bar{F}(t) dt, \\
c(w; \sigma_1) &= c_1 \frac{w}{\sigma_1} + K_d F\left(\frac{w}{\sigma_1}\right) + c_d \int_0^{\frac{w}{\sigma_1}} \left(\frac{w}{\sigma_1} - l\right) dF(l) \\
&= c_1 \frac{w}{\sigma_1} + K_d F\left(\frac{w}{\sigma_1}\right) + c_d \int_0^{\frac{w}{\sigma_1}} F(t) dt, \\
c(w; \sigma_2) &= K_2 + c_2 \frac{w}{\sigma_2} + K_d F\left(\frac{w}{\sigma_2}\right) + c_d \int_0^{\frac{w}{\sigma_2}} F(t) dt.
\end{aligned}$$

As in the general case, it can be shown that for this model there exist $v(x)$, $x \in \mathcal{X}$ and g which satisfy the average cost optimality equations (cf. (2.3)):

$$v(w) = \min \left\{ (c_1 - g) \frac{w}{\sigma_1} + K_d F\left(\frac{w}{\sigma_1}\right) + c_d \int_0^{\frac{w}{\sigma_1}} F(t) dt - g \int_{\frac{w}{\sigma_1}}^{\infty} \bar{F}(t) dt, \right. \quad (2.25)$$

$$\left. K_2 + (c_2 - g) \frac{w}{\sigma_2} + K_d F\left(\frac{w}{\sigma_2}\right) + c_d \int_0^{\frac{w}{\sigma_2}} F(t) dt - g \int_{\frac{w}{\sigma_2}}^{\infty} \bar{F}(t) dt \right\} + \int_0^{\infty} v(w) dG(w).$$

Theorem 2.3 *If $K_d = 0$ then in the restricted model π_U^* is a Control Limit Rule $CLR(m_U)$.*

Proof: If $K_d = 0$ then from (2.25) we see that σ_1 is chosen if:

$$\begin{aligned}
&K_2 + (c_2 + c_d - g) \frac{w}{\sigma_2} - c_d \int_0^{\frac{w}{\sigma_2}} [1 - F(t)] dt - g \int_{\frac{w}{\sigma_2}}^{\infty} [1 - F(t)] dt \geq \\
&(c_1 + c_d - g) \frac{w}{\sigma_1} - c_d \int_0^{\frac{w}{\sigma_1}} [1 - F(t)] dt - g \int_{\frac{w}{\sigma_1}}^{\infty} [1 - F(t)] dt \quad \Leftrightarrow \\
&K_2 - \left[\frac{c_1 + c_d - g}{\sigma_1} - \frac{c_2 + c_d - g}{\sigma_2} \right] w + (c_d - g) \int_{\frac{w}{\sigma_2}}^{\frac{w}{\sigma_1}} [1 - F(t)] dt \geq 0 \quad \Leftrightarrow \\
&H(w) \geq \bar{C}w - \bar{K}, \tag{2.26}
\end{aligned}$$

where $H(w)$ is defined by (2.17) and

$$\bar{C} := \left[\frac{c_1 + c_d - g}{\sigma_1} - \frac{c_2 + c_d - g}{\sigma_2} \right] [c_d - g]^{-1},$$

$$\bar{K} := K_2 / (c_d - g).$$

Due to Assumption 4 $\bar{K} > 0$. In Lemma B.2 (Appendix B), it is shown that

$$H(\alpha w) \geq \alpha H(w) \quad \text{for } w \geq 0 \text{ and } 0 \leq \alpha \leq 1.$$

Now suppose (2.26) is satisfied for some $m_U \geq 0$, i.e. σ_1 is chosen if $w = m_U$. Then

$$H(m_U) \geq \bar{C}m_U - \bar{K}.$$

Then using Lemma B.2, for $0 \leq \alpha \leq 1$:

$$H(\alpha m_U) \geq \alpha H(m_U) \geq \alpha(\bar{C}m_U - \bar{K}) \geq \bar{C}\alpha m_U - \bar{K}.$$

Thus,

$$\forall 0 \leq w \leq m_U : H(w) \geq \bar{C}w - \bar{K}.$$

So, if σ_1 is the optimal repair rate for some $m_U \geq 0$, then σ_1 is the optimal choice for all $0 \leq w \leq m_U$. This is exactly the definition of a Control Limit Rule (cf. Definition 2.1). \square

2.3 Counterexample: four-region policy

If $K_d > 0$ then the optimal policy in (U, w) is not always a Control Limit Rule. It may be a four-region (m_1, m_2, m_3) policy which is defined as follows:

$$\begin{aligned} &\text{if } w \in \{(0, m_1] \cup (m_2, m_3]\} \text{ then } \sigma_1 \text{ is chosen,} \\ &\text{if } w \in \{(m_1, m_2] \cup (m_3, \infty)\} \text{ then } \sigma_2 \text{ is chosen,} \end{aligned}$$

where

$$0 \leq m_1 \leq m_2 \leq m_3 < \infty.$$

The optimality of this four-region policy is intuitively argued as follows. If $w \in (0, m_1]$ then the probability of a system-breakdown is negligible. So, there is no need to switch to the fast rate σ_2 . If $w \in (m_1, m_2]$ there may be a considerable chance of a system-breakdown occurring during a slow repair, incurring fixed costs K_d . One may prevent the system from breaking down by switching to σ_2 . Then the expected down-costs are reduced such that K_2 is sufficiently compensated. If $w \in (m_2, m_3]$ then there may be a considerable chance of a system-breakdown, even when repairing at fast rate. So, in this case K_2 has to be compensated mostly by a reduction of variable repair- and down-costs. If this reduction is too small then σ_1 becomes optimal again. For $w > m_3$ the reduction of variable costs may be such that switching to σ_2 is justified.

The previous reasoning is illustrated by a small example.

$$\begin{aligned} L &\equiv 100 \text{ (deterministic),} \\ W \in \mathcal{W} &:= \{4, 104, 204, 1000\}, \\ P(W = w) &= 0.25, \quad w \in \mathcal{W}, \\ \sigma_1 &= 1, \quad \sigma_2 = 2, \\ c_1 &= 1, \quad c_2 = 2, \quad c_d = 10, \\ K_d, K_2 &> 0. \end{aligned}$$

This example inhibits all properties just mentioned. If $w = 4$ then the system will not break down, even when σ_1 is applied. If $w = 104$ then the system breaks down when σ_1 is applied, whereas the system keeps operating when σ_2 is applied. If $w = 204$ then the system breaks down, even if σ_2 is applied.

Several policies are excluded from consideration beforehand. In Theorem 2.1 we have shown that the optimal switching policy at the beginning of a down-period is of CLR-type. So, only CLR-policies are considered in state (D, σ_1, w) . Furthermore all policies that choose σ_2 in state $(U, 4)$ are non-optimal, because a fixed cost K_2 is incurred whereas no variable cost savings are made.

For each of the remaining twenty policies we have derived explicit expressions for the average cost as function of K_d and K_2 (using a regenerative approach, which is explained in Section 3.1). Now consider a four-region policy π_4 , which does never switch rates in a down state, and which chooses σ_1 in (U, w) if $w \in \{4, 204\}$ and σ_2 if $w \in \{104, 1000\}$. By comparing the average cost function of π_4 with all other average cost functions, we conclude that π_4 outperforms all Control Limit Rules if the following three conditions on K_d and K_2 are satisfied:

$$\begin{aligned} K_d &< 13026 - 27.08K_2, \\ K_d &> 1344 - 5.43K_2, \\ K_d &> 1.02K_2 - 12. \end{aligned} \tag{2.27}$$

π_4 is optimal if (2.27) is replaced by

$$K_d < 1344 - 1.90K_2.$$

Since the amount of work W is completely known to the repairman after inspection, its distribution function $G(w)$ does not have any influence on the form of the optimal policy. Note that in both the intuitive reasoning and in the example, the repair policy is tuned to the chance of the occurrence of a system breakdown, which in turn is determined by the lifetime distribution $F(l)$. We expect the optimality of a non-CLR in state (U, w) with $K_d > 0$ to depend strongly on the form of $F(l)$. If $F(l)$ is a continuous distribution function and if σ_L^2 (variance of L) deviates significantly from zero, then no accurate prediction of L can be given. In this case the long-run average cost function will be quite insensitive to the form of the repair policy applied. So, even if a non-CLR is the optimal policy, the best CLR will be close to optimal. If σ_L^2 is close to zero then it may be possible to fine-tune the repair policy to the quite deterministic lifetimes of the units such that a non-CLR is optimal.

3 Performance measures under $\text{CLR}(m_U, m_D)$

3.1 Average cost under $\text{CLR}(m_U, m_D)$

In this section we compute the long-run average cost $\text{AC}(m_U, m_D)$ of controlling our two-unit standby system by a two-dimensional Control Limit Rule $\text{CLR}(m_U, m_D)$. This formula may be useful when searching for the optimal values of m_U and m_D .

The time epochs at which one unit starts operating and an (instantaneous) inspection is carried out on the other one, are regeneration points for the system. The evolution in time of

our system can be modeled by a *regenerative process*, i.e. after every regeneration point the system evolves as if it has just been started. The time between two regeneration points is called a cycle. From the theory of regenerative processes (cf. Tijms [1986]) we know that the average cost function can be obtained from:

$$AC(m_U, m_D) := \frac{E[\text{cycle cost}]}{E[\text{cycle length}]} . \quad (3.1)$$

The expected length of a cycle is obtained from:

$$E[\text{cycle length}] := \mu_L + P\left(L < \frac{W}{\sigma}\right)E[\text{Down}], \quad (3.2)$$

where the probability of a system-breakdown within a cycle is given by:

$$P\left(L < \frac{W}{\sigma}\right) = \int_0^{m_U} F\left(\frac{w}{\sigma_1}\right)dG(w) + \int_{m_U}^{\infty} F\left(\frac{w}{\sigma_2}\right)dG(w), \quad (3.3)$$

and

$$E[\text{Down}] := \text{expected length of a system down-period},$$

which is computed in Section 3.2. The expected cost during one cycle is computed from:

$$\begin{aligned} E[\text{cycle cost}] := & c_1 E[\text{time } \sigma_1] + K_2 P(\sigma_2 \text{ is chosen}) \\ & + c_2 E[\text{time } \sigma_2] + P\left(L < \frac{W}{\sigma}\right)(K_d + c_d E[\text{Down}]), \end{aligned} \quad (3.4)$$

where $E[\text{time } \sigma_i]$ denotes the expected time the repairman is working at rate σ_i per cycle ($i = 1, 2$).

$$\begin{aligned} E[\text{time } \sigma_1] &= \int_0^{m_D} \frac{w}{\sigma_1} dG(w) \\ &+ \int_{m_D}^{m_U} \left[\int_0^{\frac{w-m_D}{\sigma_1}} l dF(l) + \frac{w}{\sigma_1} \bar{F}\left(\frac{w-m_D}{\sigma_1}\right) \right] dG(w), \\ E[\text{time } \sigma_2] &= \int_{m_D}^{m_U} \int_0^{\frac{w-m_D}{\sigma_1}} \frac{w - \sigma_1 l}{\sigma_2} dF(l) dG(w) + \int_{m_U}^{\infty} \frac{w}{\sigma_2} dG(w), \end{aligned}$$

$$P(\sigma_2 \text{ is chosen}) = \int_{m_D}^{m_U} F\left(\frac{w-m_D}{\sigma_1}\right)dG(w) + \bar{G}(m_U).$$

It is not possible to derive a closed form expression for $AC(m_U, m_D)$. After reduction, (3.2) and (3.4) have to be evaluated using some numerical routines.

3.2 Moments of system up- and down-times under $CLR(m_U, m_D)$

Often long-run average measures as defined in Section 3.1 provide insufficient information about the actual way a system will be operating. For planning purposes it may be important e.g. to be able to predict the length of an arbitrary down-period. In such situations it is useful to know

the moments (mean, variance, etc.) of system up- and down-times, which are obtainable from the corresponding Laplace transforms:

$$\phi_U(s) := \int_0^{\infty} e^{-st} P(Up > t) dt ; \quad \phi_D(s) := \int_0^{\infty} e^{-st} P(Down > t) dt , \quad s > 0.$$

Furthermore $\phi_L(s)$ denotes the Laplace transform of the lifetime distribution function. Using the regenerative nature of our system (cf. Section 3.1), in Theorem 3.1 we present a closed form expression of $\phi_U(s)$. Theorem 3.2 gives $\phi_D(s)$.

Theorem 3.1

$$\phi_U(s) = \phi_L(s) / [1 - \gamma(s)] , \quad s > 0,$$

where

$$\gamma(s) := \int_0^{\frac{m_U}{\sigma_1}} e^{-st} G(\sigma_1 t) dF(t) + \int_{\frac{m_U}{\sigma_2}}^{\infty} e^{-st} G(\sigma_2 t) dF(t) - G(m_U) \int_{\frac{m_U}{\sigma_2}}^{\frac{m_U}{\sigma_1}} e^{-st} dF(t).$$

Proof: We consider an arbitrary regeneration cycle (cf. Section 3.1) to begin at time 0 with

L := lifetime of the unit operating in that cycle,

R := repairtime of the unit under repair in that cycle.

We need the conditional probability that the repair will have been completed before the operating unit fails, given that it fails at time l ; i.e. we need the conditional repairtime distribution given that no additional opportunity to switch repair rates has occurred yet:

$$P(R \leq l \mid L = l) = P\left(\frac{W}{\sigma_1} \leq l ; W \leq m_U\right) + P\left(\frac{W}{\sigma_2} \leq l ; W > m_U\right) \quad (3.5)$$

$$= \begin{cases} G(\sigma_1 l), & \text{if } 0 \leq l \leq \frac{m_U}{\sigma_2}, \\ G(\sigma_1 l) + G(\sigma_2 l) - G(m_U), & \text{if } \frac{m_U}{\sigma_2} < l \leq \frac{m_U}{\sigma_1}, \\ G(\sigma_2 l), & \text{if } \frac{m_U}{\sigma_1} < l < \infty. \end{cases} \quad (3.6)$$

Due to the regenerative nature of our system the distribution of the length of a system up-period is obtained from:

$$\begin{aligned} P(Up > t) &= P(L > t) + \int_0^t P(R \leq l ; Up > t - l \mid L = l) dF(l) \\ &= \bar{F}(t) + \int_0^t P(R \leq l \mid L = l) P(Up > t - l) dF(l). \end{aligned}$$

Taking Laplace transforms and using (3.6) we obtain

$$\begin{aligned} \phi_U(s) &= \phi_L(s) + \int_{t=0}^{\infty} e^{-st} \int_{l=0}^t P(R \leq l \mid L = l) P(Up > t - l) dF(l) dt \\ &= \phi_L(s) + \int_{l=0}^{\infty} P(R \leq l \mid L = l) e^{-sl} \int_{t=l}^{\infty} e^{-s(t-l)} P(Up > t - l) dt dF(l) \\ &= \phi_L(s) + \phi_U(s) \int_0^{\infty} e^{-sl} P(R \leq l \mid L = l) dF(l) \\ &= \phi_L(s) + \phi_U(s) \gamma(s), \end{aligned}$$

which completes the proof of Theorem 3.1. \square

Let

$$\begin{aligned}
N(s) := & \int_0^{\frac{m_D}{\sigma_1}} e^{-st} \int_{\sigma_1 t}^{m_U} F\left(\frac{w}{\sigma_1} - t\right) dG(w) dt + \int_{\frac{m_D}{\sigma_2}}^{\frac{m_U}{\sigma_2}} e^{-st} \int_{\sigma_2 t}^{m_U} F\left(\frac{w - \sigma_2 t}{\sigma_1}\right) dG(w) dt \\
& + \int_{m_U}^{\infty} e^{-s\frac{w}{\sigma_2}} \int_0^{\frac{w}{\sigma_2}} e^{su} F(u) du dG(w) - \int_{\frac{m_D}{\sigma_1}}^{\frac{m_D}{\sigma_2}} e^{-st} dt \int_{m_D}^{m_U} F\left(\frac{w - m_D}{\sigma_1}\right) dG(w).
\end{aligned}$$

Recall from Section 3.1 that the probability of a system-breakdown occurring in a cycle is denoted by $P\left(L < \frac{W}{\sigma}\right)$, which is defined by (3.3). Now the Laplace transform of the length of a system down-period is obtained from:

Theorem 3.2

$$\phi_D(s) = N(s) / P\left(L < \frac{W}{\sigma}\right). \quad (3.7)$$

Proof: See Appendix C. \square

3.3 Additional long-run average measures under $\text{CLR}(m_U, m_D)$

Several important operational characteristics can now easily be calculated using the expressions found in Sections 3.1 and 3.2. For instance:

- $E[Up]/(E[Up] + E[Down]) :=$ availability of the system (which is the fraction of time the system is operational),
- $P(L < \frac{W}{\sigma})/E[\text{cycle}] :=$ mean number of system breakdowns occurring per time unit,
- $1/E[\text{cycle}] :=$ mean number of repairs performed per time unit,
- $\bar{G}(m_U) :=$ fraction of the total number of repairs that are fully carried out at rate σ_2 ,
- $P(\sigma_2 \text{ is chosen}) - \bar{G}(m_U) :=$ fraction of the total number of repairs that are started at rate σ_1 and completed at rate σ_2 after an intermediate switch at system-breakdown,
- $E[\text{time } \sigma_i]/E[\text{cycle}] :=$ fraction of time the repairman is working at rate σ_i , $i = 1, 2$,
- $(E[\text{cycle}] - \sum_{i=1}^{i=2} E[\text{time } \sigma_i])/E[\text{cycle}] :=$ fraction of time the repairman is idle.

4 Concluding remarks

Several questions are still open for further research.

At first, for the general model, in Theorem 2.1 we have shown that in state (D, σ_1, w) it is average cost optimal to switch to the fast repair rate σ_2 according to a CLR. For $K_d = 0$, in Theorem 2.2, we have shown that in state (U, w) the optimal repair rate is chosen according to a CLR if either $\frac{c_1}{\sigma_1} \geq \frac{c_2}{\sigma_2}$ or $F(l)$ is IFR. We conjecture, however, that in this state the optimal repair rate is chosen according to a CLR *without any restrictive conditions*, i.e. even if both $\frac{c_1}{\sigma_1} < \frac{c_2}{\sigma_2}$ and $F(l)$ is non-IFR. This conjecture is strengthened by Theorem 2.3, which proves general optimality of a Control Limit Rule in a restricted model.

Let

- m_U^G, m_D^G, g^G : the optimal Control Limits, and the minimum average costs, of the general model considered in Theorem 2.1 and 2.2.
- m_U^R, g^R : the optimal Control Limit, and the minimum average costs, of the restricted model considered in Theorem 2.3.

For $K_d = 0$, the following relationship is intuitively clear.

$$m_U^G \geq m_U^R \geq m_D^G. \quad (4.1)$$

After choosing the proper repair rate in the restricted model, it takes some time before the system eventually breaks down, thus $m_U^R \geq m_D^G$. This inequality follows easily from (2.7) and (2.26), since $g^R \geq g^G$. In the restricted model there is no additional opportunity to switch repair rates, thus we expect $m_U^G \geq m_U^R$. From (i) and (ii) in the proof of Theorem 2.2, it is immediately clear that $m_U^G \geq m_D^G$. However, we have not yet found the right arguments to prove the first inequality of (4.1).

By numerical experiments one can investigate monotonicity of the average cost function $AC(m_U, m_D)$ as a function of m_U and m_D . This result may lead to considerable savings of computation time when efficiently searching for the optimal Control Limits m_U^* and m_D^* .

Most intriguing is the form of the optimal policy for $K_d > 0$. At the end of Section 2.3 we argued that the best Control Limit Rule will be (close to) optimal if σ_L^2 deviates significantly from zero. This conjecture may be verified by numerical experiments after properly discretizing the probability distribution functions. Other questions may be answered such as: When is the best CLR a good alternative to an optimal non-CLR? What is the influence of K_d and $F(l)$ on the form of the optimal policy? Are there optimal policies with more than four regions? (We believe not) Etc.

Sensitivity results may be obtained by varying input parameters during the numerical experiments. One might for instance vary the fast repair rate, the slow repair rate, variable down costs (loss of production), or one might apply a non-optimal Control Limit Rule, etc.

Appendix A. Existence of an average cost optimal policy

In this appendix we outline the proof of the existence of an average cost optimal policy, under the additional assumption that $G(w)$ has a finite and $F(l)$ has an infinite support. First we make use of Theorem 2 of Ross [1970], which guarantees the existence of an average cost optimal policy, provided the following two conditions are satisfied:

Condition A.1 There exist finite numbers $\delta > 0$ and $\epsilon > 0$ such that

$$P(T(x; \sigma) \leq \delta) < 1 - \epsilon \quad \text{for all } x \in \mathcal{X}, \sigma \in \{\sigma_1, \sigma_2\},$$

where $T(x; \sigma)$ denotes the time until the next decision epoch, given the current state x and current action σ .

Condition A.2 There exist a bounded Baire function $v(\cdot)$ on \mathcal{X} and a constant g satisfying the optimality equation (2.3).

Theorem 2 of Ross [1970] states that under Conditions A.1 and A.2 any policy which, when in state x , selects an action minimizing the right hand side of (2.3) is average cost optimal.

Condition A.1, however, is *not* satisfied in our model, since for $i = 1, 2$

$$\inf_{x \in \mathcal{X}} \{ \tau(x; \sigma_i) \} = 0. \tag{A.1}$$

To overcome this difficulty, we slightly modify our original Semi Markov Decision Process into an equivalent Semi Markov Decision Process for which Condition A.1 does hold. This modification is based on a preliminary analysis of the average cost optimality equations (2.4) upto (2.6). Note that (A.1) is caused by those states $x \in \mathcal{X}$ which are represented by (D, σ_i, w) for small values of w ($i = 1, 2$). Hence we modify our Semi Markov Decision Process such that those states are removed from \mathcal{X} . Due to (2.6) the states (D, σ_2, w) can be removed without any difficulty for all $w \geq 0$: simply insert (2.6) into the second term of (2.4) (cf. (2.9)). Moreover, we note that σ_1 is the minimizing action in (2.5) (independently of the value of $g \geq 0$) in those states (D, σ_1, w) , with $w \leq w^*$, where

$$w^* := \frac{\sigma_1 K_2}{c_1 + c_d} > 0.$$

So by removing those states from the state space for which the optimal action can be determined on forehand, we arrive at the following modified Semi Markov Decision Process, which is equivalent to the original one (i.e. the average cost optimality equations for both models have exactly the same solutions).

$$\begin{aligned} \mathcal{X}_m &= \{ (U, w); w \geq 0 \} \cup \{ (D, \sigma_1, w); w \geq w^* \}, \\ A_m &= A_m(x) = \{ \sigma_1, \sigma_2 \}, \quad x \in \mathcal{X}_m, \end{aligned}$$

$$\begin{aligned}
\tau_m(U, w; \sigma_1) &= \mu_L + \int_0^{\frac{w}{\sigma_1}} F(t) dt, & 0 \leq w \leq w^*, \\
\tau_m(U, w; \sigma_1) &= \mu_L + \int_{\frac{w-w^*}{\sigma_1}}^{\frac{w}{\sigma_1}} \left\{ F(t) - F\left(\frac{w-w^*}{\sigma_1}\right) \right\} dt, & w > w^*, \\
\tau_m(U, w; \sigma_2) &= \mu_L + \int_0^{\frac{w}{\sigma_2}} F(t) dt, & w \geq 0, \\
\tau_m(D, \sigma_1, w; \sigma_i) &= \frac{w}{\sigma_i}, & w \geq w^*, i = 1, 2,
\end{aligned}$$

$$\begin{aligned}
c_m(U, w; \sigma_1) &= \frac{c_1 w}{\sigma_1} + K_d F\left(\frac{w}{\sigma_1}\right) + c_d \int_0^{\frac{w}{\sigma_1}} F(t) dt, & 0 \leq w \leq w^*, \\
c_m(U, w; \sigma_1) &= c_1 \left\{ \int_0^{\frac{w}{\sigma_1}} [1 - F(t)] dt + \int_{\frac{w-w^*}{\sigma_1}}^{\frac{w}{\sigma_1}} [F(t) - F\left(\frac{w-w^*}{\sigma_1}\right)] dt \right\} + \\
&\quad c_d \int_{\frac{w-w^*}{\sigma_1}}^{\frac{w}{\sigma_1}} [F(t) - F\left(\frac{w-w^*}{\sigma_1}\right)] dt + K_d [F\left(\frac{w}{\sigma_1}\right) - F\left(\frac{w-w^*}{\sigma_1}\right)], & w > w^*, \\
c_m(U, w; \sigma_2) &= K_2 + \frac{c_2 w}{\sigma_2} + K_d F\left(\frac{w}{\sigma_2}\right) + c_d \int_0^{\frac{w}{\sigma_2}} F(t) dt, & w \geq 0, \\
c_m(D, \sigma_1, w; \sigma_1) &= K_d + (c_1 + c_d) \frac{w}{\sigma_1}, & w \geq w^*, \\
c_m(D, \sigma_1, w; \sigma_2) &= K_d + K_2 + (c_2 + c_d) \frac{w}{\sigma_2}, & w \geq w^*.
\end{aligned}$$

Finally the one-step transition probabilities are given by

$$\begin{aligned}
p_m\{(U, [0, v]) | (U, w; \sigma_1)\} &= G(v), & 0 \leq w \leq w^*, \\
p_m\{(U, [0, v]) | (U, w; \sigma_1)\} &= G(v)[1 - F\left(\frac{w-w^*}{\sigma_1}\right)], & w \geq w^*, \\
p_m\{(U, [0, v]) | (U, w; \sigma_2)\} &= G(v), & w \geq 0, \\
p_m\{(D, \sigma_1, [w - \sigma_1 t, w]) | (U, w; \sigma_1)\} &= F(t), & w \geq w^*, 0 \leq t < \frac{w-w^*}{\sigma_1}, \\
p_m\{(U, [0, v]) | (D, \sigma_1, w; \sigma_i)\} &= G(v), & w \geq w^*, i = 1, 2.
\end{aligned}$$

Note that for this modified Semi Markov Decision Process the transition times $T_m(x; \sigma)$ between two successive decision epochs have the property

$$T_m(x; \sigma) \geq \min \left\{ L, \frac{w^*}{\sigma_2} \right\}, \quad \text{for all } x, \sigma.$$

Since $F(0) = 0$, Condition A.1 is certainly satisfied for the modified model. To verify Condition A.2 for the modified model, we invoke Theorem 3.1 in Kurano [1985], which states that Condition A.2 holds if the Conditions A.3 and A.4 below are fulfilled.

Condition A.3 The one-step transition functions $\tau_m(x; \sigma)$ and the one-step cost functions $c_m(x; \sigma)$ are bounded on $\mathcal{X}_m \times A_m$.

Condition A.4 There exists a finite measure γ on \mathcal{X}_m and a $0 < \beta < 1$ such that

- (i) $p_m\{ \mathcal{B} \mid (x; \sigma) \} \geq \tau_m(x; \sigma)\gamma(\mathcal{B})$ for any Borel set \mathcal{B} of \mathcal{X}_m ,
- (ii) $\gamma(\mathcal{X}_m) > (1 - \beta)/\tau_m(x; \sigma)$ for any $(x; \sigma) \in \mathcal{X}_m \times A_m$.

Condition A.3 is trivially satisfied under the following assumption.

Assumption 5 $G(w)$ has finite support $[0, w_{max}]$ and $F(l)$ has infinite support.

Note that Assumption 5 implies that the state space \mathcal{X}_m can be restricted to the states (U, w) and (D, σ_1, w) with $w \leq w_{max}$.

From the specification of the one-step transition functions $\tau_m(x; \sigma)$ and the one-step transition probabilities $p_m\{ \cdot \mid (x; \sigma) \}$ it is straightforwardly verified that the following choices for the measure $\gamma(\cdot)$ and the number β satisfy Condition A.4.

$$\begin{aligned} \gamma(U, [0, v]) &= \frac{G(v) \left[1 - F\left(\frac{w_{max}}{\sigma_1}\right) \right]}{\tau_{max}}, & v \geq 0, \\ \gamma(D, \sigma_1, [0, w]) &= 0, & w \geq 0, \end{aligned}$$

and

$$1 - \beta = \frac{\tau_{min}}{\tau_{max}},$$

where

$$\tau_{min} := \inf_{x, \sigma} \{ \tau(x; \sigma) \} \quad \text{and} \quad \tau_{max} := \sup_{x, \sigma} \{ \tau(x; \sigma) \}.$$

The exposition above yields

Theorem A.1 *Under Assumption 5 Equation (2.3) has a bounded solution, and any policy which, when in state x , selects an action minimizing the right hand side of (2.3) is average cost optimal. \square*

Appendix B. Auxiliary lemma's to Theorem 2.2 and 2.3

Let $H(w)$ be defined by (2.17).

Lemma B.1 *If $F(l)$ is IFR then $H(w)$ is unimodal.*

Proof: Since $H(w) = 0$ if $F(\frac{w}{\sigma_2}) = 1$, and $H(w)$ is monotonically decreasing if $F(\frac{w}{\sigma_2}) < 1$ and $F(\frac{w}{\sigma_1}) = 1$, we only consider w such that $F(\frac{w}{\sigma_1}) < 1$. From (2.17) and (2.21) we note that:

$$H(0) = 0; \quad H'(0) > 0; \quad H(\infty) = 0.$$

So, there is at least one solution to the following equation:

$$H'(w) = 0. \tag{B.1}$$

$H(w)$ is unimodal iff (B.1) has a unique solution. For convenience we assume:

$$\sigma_1 = 1; \quad \sigma_2 > 1.$$

Now (B.1) is equivalent with

$$Q(w) := \frac{1 - F(w)}{1 - F(\frac{w}{\sigma_2})} = \frac{1}{\sigma_2}. \tag{B.2}$$

Since

$$Q(0) = 1 > \frac{1}{\sigma_2},$$

a solution to (B.2) is unique if

$$Q'(w) < 0 \quad \Leftrightarrow$$

$$\frac{1}{\sigma_2} \frac{f(\frac{w}{\sigma_2})}{[1 - F(\frac{w}{\sigma_2})]} < \frac{f(w)}{1 - F(w)},$$

which is satisfied if $F(l)$ is IFR. □

Lemma B.2

$$H(\alpha w) \geq \alpha H(w), \quad w \geq 0; \quad 0 \leq \alpha \leq 1.$$

Proof:

$$\begin{aligned} \alpha H(w) &= \int_{\frac{w}{\sigma_2}}^{\frac{w}{\sigma_1}} \alpha [1 - F(t)] dt \\ &\leq \int_{\frac{w}{\sigma_2}}^{\frac{w}{\sigma_2} + \alpha(\frac{w}{\sigma_1} - \frac{w}{\sigma_2})} [1 - F(t)] dt \\ &\leq \int_{\frac{\alpha w}{\sigma_2}}^{\frac{\alpha w}{\sigma_1}} [1 - F(t)] dt = H(\alpha w). \end{aligned}$$

□

Appendix C. Proof of Theorem 3.2: $\phi_D(s)$.

Consider an arbitrary regeneration cycle to begin at time 0. Let

$$\begin{aligned}\sigma &:= \text{initial repair rate,} \\ \sigma' &:= \text{repair rate after system-breakdown.}\end{aligned}$$

The distribution of the length of a system down-period is given by:

$$\begin{aligned}P(\text{Down} > t) &= P\left(\frac{W-\sigma L}{\sigma'} > t \mid L < \frac{W}{\sigma}\right) \\ &= P\left(\frac{W-\sigma L}{\sigma'} > t\right) / P\left(L < \frac{W}{\sigma}\right).\end{aligned}$$

$P\left(L < \frac{W}{\sigma}\right)$ is obtained from (3.3). Let the indicator function $I(a > b)$ with $a, b \in \mathbb{R}$ be defined by

$$I(a > b) = \begin{cases} 1 & \text{if } a > b \text{ (true),} \\ 0 & \text{otherwise (false).} \end{cases}$$

Now:

$$\begin{aligned}P\left(\frac{W-\sigma L}{\sigma'} > t\right) &= \int_0^{m_U} P\left(\frac{w-\sigma_1 L}{\sigma'} > t\right) dG(w) + \int_{m_U}^{\infty} P\left(\frac{w-\sigma_2 L}{\sigma_2} > t\right) dG(w) \\ &= A(t) + B(t) + C(t),\end{aligned}$$

where $A(t)$, $B(t)$ and $C(t)$ are defined by:

$$A(t) := \int_0^{m_U} \int_{\frac{w-m_D}{\sigma_1}}^{\frac{w}{\sigma_1}} I\left(\frac{w}{\sigma_1} - l > t\right) dF(l) dG(w),$$

$$B(t) := \int_{m_D}^{m_U} \int_0^{\frac{w-m_D}{\sigma_1}} I\left(\frac{w-\sigma_1 l}{\sigma_2} > t\right) dF(l) dG(w),$$

$$C(t) := \int_{m_U}^{\infty} P\left(L < \frac{w}{\sigma_2} - t\right) dG(w).$$

Careful inspection of $A(t)$, $B(t)$ and $C(t)$ leads to the following expressions:

$$A(t) = \begin{cases} \int_{\sigma_1 t}^{m_U} F\left(\frac{w}{\sigma_1} - t\right) dG(w) - \int_{m_D}^{m_U} F\left(\frac{w-m_D}{\sigma_1}\right) dG(w) & \text{if } 0 \leq t < \frac{m_U}{\sigma_1}, \\ 0 & \text{if } t \geq \frac{m_U}{\sigma_1}, \end{cases}$$

$$B(t) = \begin{cases} \int_{m_D}^{m_U} F\left(\frac{w-m_D}{\sigma_1}\right) dG(w) & \text{if } 0 \leq t < \frac{m_D}{\sigma_2}, \\ \int_{\sigma_2 t}^{m_U} F\left(\frac{w-\sigma_2 t}{\sigma_1}\right) dG(w) & \text{if } \frac{m_D}{\sigma_2} \leq t < \frac{m_U}{\sigma_2}, \\ 0 & \text{if } t \geq \frac{m_U}{\sigma_2}, \end{cases}$$

$$C(t) = \begin{cases} \int_{m_U}^{\infty} F\left(\frac{w}{\sigma_2} - t\right) dG(w) & \text{if } 0 \leq t < \frac{m_U}{\sigma_2}, \\ \int_{\sigma_2 t}^{\infty} F\left(\frac{w}{\sigma_2} - t\right) dG(w) & \text{if } t \geq \frac{m_U}{\sigma_2}. \end{cases}$$

$\phi_D(s)$ can now be obtained by integrating over the appropriate regions for t :

$$\phi_D(s) = \int_0^{\infty} e^{-st} [A(t) + B(t) + C(t)] dt / P\left(L < \frac{W}{\sigma}\right),$$

which gives (3.7). □

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